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Development and Fabrication of Small Capacity Garlic Peeler

Maninder Kaur*, Preetinder Kaur and Mahesh Kumar

Department of Processing and Food Engineering, Punjab Agricultural University, Ludhiana, Punjab, India

*Corresponding author

ABSTRACT

Keywords

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Garlic (*Allium sativum* L.) is one of the most perennial bulb crops of Liliaceae family. It is widely used as a condiment and for medicinal and pharmaceutical preparations. Traditional methods of garlic peeling are laborious, time and cost intensive. The present study was undertaken to develop and evaluate the performance of small capacity garlic peeler so as to overcome the time consumption and cost intensiveness. Engineering properties of garlic relevant to peeler development were identified and measured. It worked on the abrasion principle with very little damage to the cloves after peeling. The peeler was analyzed for its performance at different roller speeds and pretreatment conditions. An evaluation of the performance of the developed peeler with hot air pretreated cloves indicated that it recovered 39.40% of peeled cloves after peeling at 400 rpm of roller speed. For the control samples, maximum peeled clove recovery was 33.45%. The capacity of the machine was found to be 15 kg/h. The maximum peeling efficiency observed was 48.13% with hot air pretreated samples peeled at 400 rpm of roller speed. An economic analysis indicated that the developed garlic peeler could be profitably used for the small scale peeling operations.

Introduction

Garlic (*Allium sativum* L.), the spice of human life, is one the most important perennial bulb crops of the lily family (Liliaceae) which is grown all over the plains of India and is used as a condiment throughout the country. India ranks second after China in world's garlic production and contribute 14% of the world area. According to National Horticulture Database (2011), the total production of spices in India during 2010-2011 was 5351 thousand

million tonnes from an area of 2940 thousand hectares giving productivity of 1.8 MT/ha. The share of area under garlic is 200.60 thousand hectare with productivity of 53MT/ha. During the same period, Punjab produced 63.5 thousand million tonnes from an area of 18.4 thousand hectares, giving the productivity of 3.5 MT/ha. Punjab ranks first with the highest yield at 14.73 tonnes / ha.

Fresh garlic is characterized as having a distinct aromatic odour which is seldom

carried over into processed garlic (Pezutti and Crapsite 1997). The flavour of garlic is attributed to the sulfur containing volatiles. By the action of an enzyme allinase, allyl -S-cysteine sulfoxide (allin) is converted to diallyl thiosulfonates (allicin) and then disproportionates to disulfides and thiosulfonates.

Garlic is valued for its flavor and has an extensive commercial importance because of its wide medicinal value and application in food and pharmaceutical preparations (Sharma and Prasad, 2001). It has been recognized as a valuable food condiment in everyday cooking. Garlic is commonly processed into dehydrated powder, flakes and slices (Ahmad 1996). This involves a cumbersome unit operation of peeling. With changing lifestyles, people are moving towards readily available processed products. During garlic peeling the thin membrane skin is to be removed off from the segments. Various methods such as lye peeling, hot water blanching, oven peeling, flame peeling etc are used for peeling the garlic. In lye peeling method, garlic is immersed in hot caustic soda solution in the lye peeler itself followed by vigorous water rinse to remove the chemicals adhered to the skin. The cloves are then neutralized in acid bath and trimmed to give perfect finish. Hot water blanching is a traditional method of peeling that involves the submergence of cloves in warm water for 5-10 minutes. The outer skin gets softened and can be easily peeled by hand. In the oven method of peeling, garlic is placed in oven for 5-10 seconds. The root is then cut and skin slides off easily. Flame peeling is another tedious method in which garlic is brought into direct contact with the live flame. High temperature burns the outer skin and can be easily removed.

Commonly available mechanical peeling methods involve the use of abrasion gadgets.

These have been found infeasible as the cloves are crushed during the process (Mudgal *et al.*, 1998). At present, there is need to develop efficient processing and peeling equipments for the garlic cloves. For this, the knowledge of basic engineering and physical properties of garlic is necessary for the development and fabrication of equipments and machinery.

A number of researchers have worked on the physical properties of garlic (Madamba *et al.*, 1993, 1995, 1997; Pezutti and Crapsite 1997; Park *et al.*, 1981; Bhatt *et al.*, 1998; Sharma and Prasad 2002) but the literature on the development of garlic clove peeler is somewhat limited. Madamba *et al.*, (1993) measured the length, width and thickness of garlic slices by using Vernier caliper. Song and Litch-field (1991) measured the length, width and thickness of garlic slices by using a computer imaging system while using a caliper to measure the third dimension.

Suwat Tansiri (1998) designed and developed the machine with 1200 x 1900 x 1900 mm (WLH) in dimensions consisting of three main units: processing from garlic bulbs to garlic cloves unit, sorting unit and peeling unit, using 3 hp motor as power source. The peeling capacity of the machine is 33.19 kg/hr, 11.02% of completely peeled off garlic flesh, 11.25% of partly peeled off garlic fresh. Nagarajan (2006) developed a garlic peeling machine with a capacity 200 kg/h. The pressurized air pushed the garlic entering the peeling chamber from the big blower to the rotating blade. Since the blades were rotating, they hit the garlic towards the serrated wall of the peeling and it gets peeled. Mudgal and Chapawat (2008) tested the performance of an air-assisted garlic clove peeler. The height of the peeling chamber (400 mm), bed depth (60 mm), air jet pressure (10, 15 and 20 kg/cm²) and position of air jet (60, 80 and 90 mm) were taken for evaluation. The peeling efficiency was observed to be 97-98%.

Manjunatha *et al.*, (2012) developed a power operated garlic peeler having cylinder concave mechanism. The cylinder covered with 10 mm thick rubber was fabricated and evaluation was done with cylinder speed (29, 36 and 42 rpm), cylinder concave clearance (8, 10 and 12 mm), moisture content (23.1, 27.7, 33.4 and 40.5% wet basis) and concave mechanisms. The peeling efficiency, yield of peeled garlic and unpeeled garlic, damage and peel separation were 86.6, 86.2, 4.7, 9.15 and 9.6% respectively at optimized parameters of cylinder speed of 36 rpm, cylinder concave clearance of 10 mm, mild steel square (8×8 screen). The machine had a throughput capacity of 27 kg/hr and energy requirement of 1.15 kw-h.

At present, the process of garlic peeling is done mostly manually which is a laborious operation. In order to overcome this and to accelerate the peeling operation, the study on the fabrication of small capacity garlic peeler was undertaken.

Design considerations

Determination of moisture content

The hot air oven method (AOAC 2000) was used to determine the moisture content of garlic cloves in which 5 gram sample was placed in dried petri-dish in a hot air oven. The operating temperature was $100 \pm 5^\circ\text{C}$ until the constant weight was obtained. The fresh and bone dried sample was weighed with the help of electronic balance (Universal weighing machine) with a sensitivity of 0.001g (1.200 kg capacity). The moisture content reported was on % wet basis. The moisture content was calculated using the following relationship:

$$\text{Moisture content (\% wb)} = \frac{\text{Wet weight} - \text{Bone dry weight}}{\text{Wet weight}} \times 100$$

Determination of engineering properties of garlic

The present study represents the evaluation of various engineering properties of both peeled and unpeeled garlic cloves. The physical properties such as length, width and thickness were measured to estimate the geometric mean diameter and sphericity. For purpose, random sampling of garlic cloves was done in which 10 groups of samples consisting of 100 segments were selected to measure the three basic dimensions using a digital Vernier caliper with an accuracy of 0.01 mm (Madamba *et al.*, 1993). Geometric mean diameter (D_p) and sphericity (ϕ) were calculated using the formulas (Mohsenin, 1986).

$$D_p = (abc)^{1/3}, \phi = (abc)^{1/3} / a$$

Frictional properties such as static coefficient of external friction and coefficient of internal friction were determined against two surfaces one wooden and other galvanized iron. These are helpful in design of bins, hopper and conveyers. A tilting table top set up consisting of wooden plank fixed on two adjustable screws was used. The formula used was

$$\mu = (W_2 - W_1) / W$$

Where, W_1 – weight to cause sliding of box when empty, W_2 – weight to cause sliding of box filled with sample material, W - weight of material in the box

Angle of repose is another physical property for describing the angle of hopper. The apparatus consists of conical hopper mounted above a circular base plate and a scale was attached to measure the height of heap. Angle of repose was determined using the following formula (Mohsenin, 1986).

$$\phi_r = \tan^{-1}(2h / D_b)$$

Where, h- height of heap (cm), D_b – Diameter of the base plate (cm).

In order to determine the bulk density of cloves, a container or cylinder of known volume was used along with electronic balance and was calculated using the relationship:

$$p_b = M/V$$

Where p_b - bulk density, M- mass of the sample in grams, V- Volume of the same sample in cc.

The garlic segment volume (V) and true density (p_p) was determined using the liquid displacement method (Mohsenin, 1970; Sitkei, 1976; Singh and Goswami, 1996). Measuring cylinder was filled with toluene and known weight of cloves was poured.

The difference in the level of the toluene before and after pouring gave the volume of toluene displaced. The formula used for the calculation was:

$$p_p \text{ (g/cc)} = W / (V_2 - V_1)$$

Where W – weight of sample in grams, V_2 – Volume of cylinder after pouring the cloves (cc), V_1 - Volume of cylinder before pouring the cloves(cc). The porosity (ϵ) of cloves was calculated by using the following relationship which was expressed as in percentage from the bulk density and true density (Jha 1999).

$$\epsilon = (p_p - p_b) \times 100 / p_p$$

Design and fabrication of garlic peeler

A small capacity power operated garlic peeler was fabricated consisting of hopper, wooden roller, cylindrical cover, blower and power transmission unit (Fig. 1 and 2). The peeler works on abrasion principle. The details of the fabricated parts are given in Table 4.

Hopper

Feeding hopper was made of MS sheet (22 gauge) with rectangular opening at the top and trapezoidal bottom. The feeding angle was designed taking into account the angle of repose of garlic.

The hopper was attached to the cylindrical unit to convey the feed under the gravitational force. The specifications of the hopper are as mentioned below.

Upper part (L×W) = (30×23) cm, Lower part (L×W) = (17×9) cm, Height of the hopper = 16 cm

Angle of repose is calculated using the formula, $(\phi_r) = \tan^{-1}(H/B)$

Where, H is the height of hopper and B is the effective base.

Here, H is 16 cm and B is (30 -17) cm. Using the formula, $\phi_r = \tan^{-1}(16/13) = 50.90$ degrees.

Roller and cylindrical unit

Roller and cylindrical unit consisted of wooden roller, outer cylindrical cover and an abrasive material. Wooden roller of 130 mm diameter and 210 mm length was prepared out of teak log of wood. The roller rotates over the MS rod (460 mm in length and 25.4 mm in diameter) driven by the power transmission unit. Nylon brushes of 40 mm length were fixed on the wooden roller with shoe nails.

Torque transmitted to the peeling chamber was calculated using the formula:

$$hp = \frac{2 \pi NT}{60}$$

Where hp is the horsepower, N is the rpm of roller.

Maximum and minimum torque transmitted to the roller was calculated

Case 1- For maximum RPM = 500

$$2\pi NT \div 60$$

hp =

1 hp motor was used for the rotation of roller and 1hp = 746 watts

$$\frac{60 \times 746}{2\pi \times 500}$$

So T = 14.247 N-m

Case 2- For minimum RPM = 300

$$\frac{60 \times 746}{2\pi \times 300}$$

So T = 23.745 N-m

Shearing stress on the rod

$$\tau = \frac{16 \times T \times 1000}{\pi d^3}$$

Where T is the torque in N-m and d is the diameter of the rod in mm

Maximum shearing stress, τ

$$= \frac{16 \times 23.745 \times 1000}{\pi \times (25.4)^3} = 7.379 \text{ N/mm}^2$$

Minimum shearing stress, τ

$$= \frac{16 \times 14.247 \times 1000}{\pi \times (25.4)^3} = 4.427 \text{ N/mm}^2$$

Moment of inertia of the rod (mm⁴)

$$I = \frac{\pi \times d^4}{64}$$

Where d is the diameter of MS rod in mm.

Therefore, I = $\frac{\pi \times (25.4)^4}{64} = 20431.71 \text{ mm}^4$

Bending moment of the shaft

$$M_b = \frac{E \times I}{r}$$

Where E is the modulus of elasticity in N/mm², I is the moment of inertia in mm⁴ and r is the radius of MS rod (E= 200N/m² for mild steel).

$$M_b = \frac{2 \times 20431.71}{12.7 \times 10000} = 0.321 \text{ N-mm}$$

The wooden roller was covered with cylindrical unit divided into two hemispherical sections. The length, width and height of the hemispherical section was designed as 280 mm, 235 mm and 175 mm respectively. The cylindrical unit was fabricated out of MS sheet (22 gauge). From inside, the cylindrical cover was lined with nylon abrasive mat which was fixed with 3/16 zisti nut and bolt.

The clearance between the abrasive material and roller was adjustable and was adjusted to ½ inch. The whole unit was installed below the feed hopper and beneath was supported by the main frame of the machine. The upper hemispherical part of the cylinder is movable with the help of jointer in order to facilitate the cleaning process.

Driving mechanism

The roller was driven by V- belt (B-30) drive to transmit the power. Two pulleys (A section with 650 mm diameter), one roller pulley and other motor pulley were used to transmit the power from one point to other with the help of belt.

No gear reduction was done at the driver and driven pulleys. Two bearings of P-204 were provided at the ends of the shaft for smooth and frictionless running of the shaft.

Power mechanism

A single phase DC motor was used as a power source with the following specifications. A variable speed control panel was attached to vary the RPM of the roller. Energy consumption was measured from the single phase energy meter attached to the machine.

Cleaning and discharge section

Peel separation and discharge of peeled and unpeeled mixture takes place at the bottom side of the cylinder. Peel separation was done with ¼ hp single phase blower and was driven with 1 hp motor. The separation of the peeled and unpeeled cloves was done manually and was fed again into hopper for peeling.

Main frame

The main frame was fabricated out of angle iron of ¼ inch × 6 mm for mounting the different parts such as roller, cylinder unit, cleaning, discharge section and transmission unit. The length, width and height of the frame were 630 mm × 470 mm × 960 mm respectively.

Experimental evaluation of small scale garlic peeler

Material

To accomplish the selected objectives, the experiments were conducted in various laboratories of the Department of Processing and Food Engineering, Punjab Agricultural University, Ludhiana. Fresh garlic was procured from the local market and was stored at ambient air conditions.

Pretreatment

Garlic samples were pretreated with hot water and hot air. Hot water treatment was given by

dipping the cloves in water heated at 90°C for 2 minutes. Hot air pretreatment was given by heating the samples in convective tray drier at 60°C for an hour with air velocity of 1m/s (Manjunatha *et al.*, 2012).

Performance evaluation of garlic peeler

The machine was tested for its peeling efficiency at different levels of roller speed and different moisture contents of pretreated and control samples. For testing the effectiveness, 1/2 kg of batch sample was fed into the hopper and time required for each peeling was noted. Corresponding weight of peeled, unpeeled, damaged and peel was noted done by weighing on electronic balance. Percentages of various fractions were obtained by using the following formulae.

$$\text{Percentage of peeled cloves} = \frac{W_p}{W_p + W_u} \times 100$$

Where W_p – weight of peeled cloves, W_u – weight of unpeeled cloves

$$\text{Percentage of unpeeled cloves} = \frac{W_u}{W_p + W_u} \times 100$$

Where W_p – weight of peeled cloves, W_u – weight of unpeeled cloves

$$\text{Percentage peeled clove recovery} = \frac{W_p}{W} \times 100$$

Where W_p – weight of peeled cloves, W – weight of garlic cloves

Machine peeling capacity

$$C_p = \frac{L_b}{(T_1 + T_2 + T_3) \times 1000} \text{ ton/hr}$$

T_1 = loading time in minutes, T_2 = peeling residence time in minutes, T_3 = unloading time in minutes, L_b = batch load (kg).

Statistical analysis

The analysis of performance evaluation of machine and effect of pretreatments on the peeling efficiency and peeled clove recovery was done using two way ANOVA technique (SAS software) and GraphPad PRISM Version 6 software, Inc. USA. The Results of analysis were used to evaluate the significant difference among the various parameters at $p < 0.05$.

Results and Discussion

Engineering properties

The values of average length, width and thickness were determined for both peeled and unpeeled cloves. From these, the average values of geometric mean diameter were found to be 11.820 mm and 11.048 mm respectively for unpeeled and peeled cloves. Forb the peeled cloves, the maximum average length, width and thickness was found to be 22.579 mm, 9.58 mm, 7.815 mm (Table 1). Similar results for the length, width, thickness and geometric mean diameter were reported by Haciseferogullari *et al.*, (2005). The values reported were 14.46 ± 0.437 , 9.25 ± 0.240 and 15.15 ± 0.285 mm respectively for the garlic (whole and segments) at 66.32% moisture content on dry basis.

The sphericity values for the unpeeled and peeled cloves were found to be 0.494 and 0.526. Higher the sphericity values, the shape approaches more towards a sphere. So, the peeled cloves exhibit sphere like character. Masoumi *et al.*, (2006) reported that sphericity values lied in the range of 0.58 – 0.91 for white and 0.57 -0.87 for pink garlic cloves at 42.4% moisture content on wet basis.

The average values of static coefficient of friction for unpeeled and peeled cloves were calculated as 0.366 and 0.772 respectively for wooden and GI surface. For the peeled cloves, the average values for the wooden and GI surface was found to be 0.664 and 0.812 respectively (Table 2). The values for the peeled cloves were reported higher than that of unpeeled cloves because of reduction in the surface smoothness of peeled cloves. The maximum values of static coefficient were reported of peeled cloves for GI surface with value of 0.812.

The efforts made by other researchers showed that the static coefficient of friction values were near to values reported in the present study. The surfaces used were galvanized sheet, iron sheet and plywood and the corresponding values for the garlic segments were 0.416 ± 0.018 , 0.472 ± 0.023 and 0.541 ± 0.028 respectively (Haciseferogullari *et al.*, 2005).

The peeled cloves have less angle of repose because of lower moisture content and the values for unpeeled cloves was 39.881 degrees and for the peeled cloves was 25.529 degrees. Similar, trend was shown by Haciseferogullari *et al.*, (2005) for the angle of repose of segments which increased from 25.5 to 37.5 degrees with increase in moisture content from 23.1 to 40.5% wet basis. It could be attributed to the increase in cohesiveness between the garlic segments.

The bulk density determined using the standard method was found to be 0.471 g/cc and 0.556 g/cc for the unpeeled and peeled cloves respectively (Table 3). Haciseferogullari *et al.*, (2005) reported the bulk density of garlic segments as 0.479 g/cc. True density was calculated using toluene displacement method. The average values reported were 1.077 g/cc and 1.169 g/cc for the unpeeled and peeled cloves respectively.

Fig.1 Schematic view of developed peeler

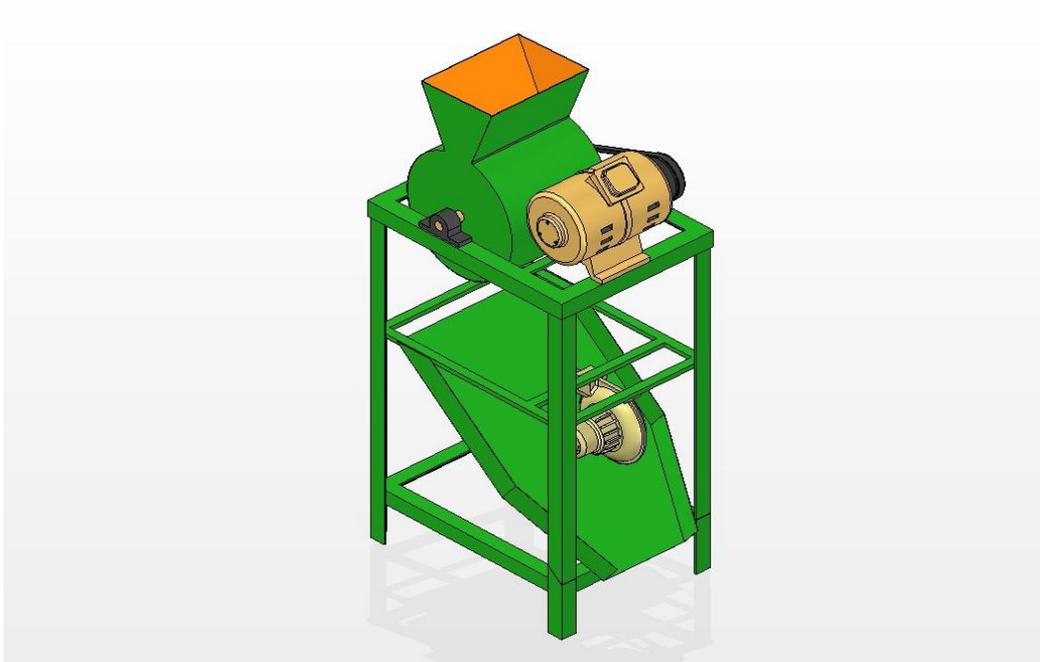


Fig.2 Actual view of developed peeler



Fig.3 Peeling efficiency as affected by roller speed and pretreatment

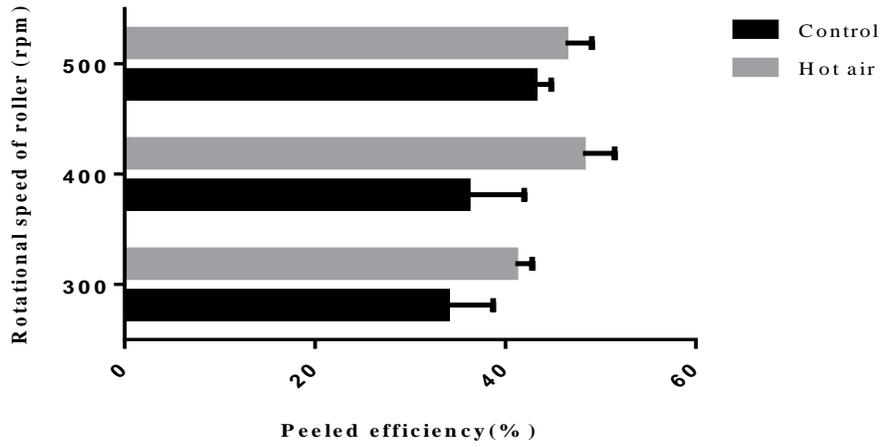


Fig.4 Effect of rotational speed and pretreatment on peeled clove recovery

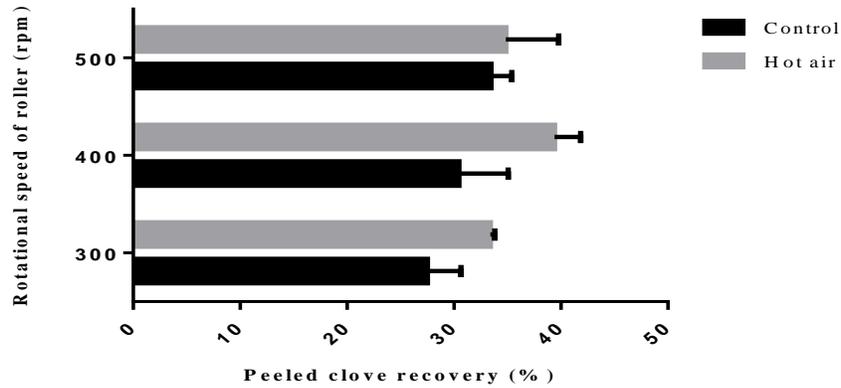


Fig.5 Control sample after peeling in the peeler



Fig.6 Hot air pretreated sample after peeling



Table 1 Average values (\pm SD) of dimensions, geometric mean diameter and sphericity of unpeeled and peeled cloves.

Property	Treatment	
	Unpeeled	Peeled
Average length, a (mm)	23.882 (4.747)	21.002 (3.087)
Average width, b (mm)	9.423 (1.414)	9.053 (1.622)
Average thickness, c (mm)	7.331 (0.987)	7.168 (1.285)
Geometric mean diameter,		
Dp (mm)	11.820 (1.207)	11.048 (1.552)
Sphericity, ϕ	0.494 (0.061)	0.526 (0.189)

Table 2 Average values of coefficient of friction for wooden surface and GI sheet.

Property	Type of surface	Garlic samples	
Coefficient of external friction	Wooden	Peeled (μ_e)	Unpeeled (μ_e)
		0.664	0.366
	GI sheet	0.812	0.772
Coefficient of internal friction		0.570	0.826

Table 3 Average values (\pm SD) of other engineering properties of unpeeled and peeled cloves.

Property	Treatment	
	Unpeeled	Peeled
Bulk density (g/cc)	0.471 (0.007)	0.556 (0.019)
True density(g/cc)	1.077 (0.067)	1.169 (0.038)
Porosity (%)	56.179 (3.027)	52.413 (1.899)

Table.4 Components of the machine

Components	Specifications
Hopper	
Material	MS Sheet (22 gauge)
Dimensions of upper part (L×W)	30 × 23(cm)
Dimensions of lower part (L×W)	17× 9(cm)
Height from the base of hopper	16 cm
Roller	
Material	Wood
Diameter	130 mm
Length	210 mm
Shaft	
Material	Mild steel
Length	460 mm
Diameter	254 mm
Nylon brushes	
Number of brushes	4
Length of each brush	40 mm
Cylindrical Cover with two hemispherical halves	
Material	MS flat sheet (22 gauge)
Length	280mm
Width	235mm
Height	175mm
Belt	B- 30 V belt
Pulleys for power transmission	
Motor and roller pulley	
Type	A type, 2 in number
Diameter	650 mm
Bearings	
Material	Gun metal
Type	P-204
Number	2
Power Mechanism	
Motor	Single phase, DC
Hp	1
Volts	220
AMP's	4
Maximum RPM	1500
Duty	Cont
Winding	Shunt
Cleaning unit	
Blower Power	¼ hp single phase driven by 1 hp motor
Main frame	
Material	Angle iron (1/4inches × 6 mm)
Length	630 mm
Width	470 mm
Height	960 mm

Table.5 Economic analysis

Assumptions	Values
1. Working hours/day	= 10
2. No. of working days in a year	= 150
3. Weight of the material in one batch	= 15 kg
4. 100 kg of raw material yield	= 46.8 kg of peeled cloves
Total cost	
<i>Fixed annual cost</i>	
Total fixed investment	= Rs. 19000
Depreciation (10%)	= Rs. 1900
Interest (12%)	= Rs. 228
Total	= Rs. 2128
<i>Variable cost</i>	
Cost of raw material	= Rs. 90/kg
Total amount of raw material processed	= 15 x 10
	= 150 kg/day
Total cost of producing raw material	= 150 x 150 x 90
	= Rs. 2025000
Maintenance cost	= 1% of fixed investment
	= Rs. 190
Cost of unskilled worker/year	= Rs. 22000
Electricity consumption @ Rs.6/unit	= Rs. 72x150
	= Rs. 10800
Miscellaneous	= Rs. 500
Total variable cost per year	= Rs. 2057990
Total cost of project year	= Rs. 2057990 + 2128
	= Rs. 2060118
Returns	
Total material processed	= 216 x 180
(Assuming 10% losses)	= 20250 kg
Total cloves peeled	= 20250 x 0.468
	= 9477 kg
Selling price of peeled cloves	= Rs. 220/kg
	= Rs. 2084940
Gross profit	= Rs. 24822/year
	= Rs. 2068.5/month
Break Even Point	
It was determined by using the following formula	
$B = \frac{F}{P - V}$	
where,	
B =	Break even point in terms of quantity of material processed annually
F =	Total annual fixed cost = Rs. 2128
V =	Variable cost/kg of the material processed = Rs. 101.63
P =	Returns per kg of the material processed including returns from byproducts, if any
	= 0.468 x 220
	$\frac{2128}{0.468 - 101.63}$
= Rs. 102.96/kg	= 1.33
= 1600	
Payback period	
It was determined by the formula	
$= \frac{\text{Capital investment}}{\text{Annual profits} + \text{Depreciation}}$	
	$= \frac{19000}{24822 + 1900} = 0.711 \text{ years}$
	$= 259.5 \text{ days} \approx 9 \text{ months}$

Table 6 Analysis of variance (ANOVA) for peeling efficiency

Source	DF	Type III SS	Mean Square	F Value	Pr > F
Pretrtmnt	1	2108.777216	2108.777216	121.80	<.0001
Rolr_Speed	2	102.740622	51.370311	2.97	0.0706
Pretrtmnt*Rolr_Speed	2	259.516368	129.758184	7.49	0.0030

Table 7 Analysis of variance for peeled clove recovery

Source	DF	Type III SS	Mean Square	F Value	Pr > F
Pretrtmnt	1	608.2202133	608.2202133	38.82	<.0001
Rolr_Speed	2	429.7433600	214.8716800	13.71	0.0001
Pretrtmnt*Rolr_Speed	2	354.9316267	177.4658133	11.33	0.0003

Masoumi *et al.*, (2006) studied the relationship between porosity and moisture content of white and pink garlic cloves. The porosity decreased from 59 to 45% and 57 to 39% for white and pink garlic cloves when the moisture content increased from 34.9 to 56.7 % wet basis. For the unpeeled cloves, the value of porosity was 56.17% and for the peeled cloves was 52.43%.

Machine peeling capacity

Machine peeling capacity was calculated using the formula of Ghobashy *et al.*, (2012).

$$C_p = \frac{L_b}{(T_1 + T_2 + T_3) \times 1000} \text{ ton/h}$$

Here, T₁ = 0.5 min, T₂ = 1 min, T₃ = 0.5 min and L_b = 0.5 kg, so C_p = 0.015 ton/h.

Calculation of peeling efficiency and peeled clove recovery

Effect of pretreatment on peeling efficiency

Two types of garlic samples, control and hot air blanched were evaluated for peeling

efficiency at different levels of 300, 400 and 500 roller speeds. The corresponding moisture contents of control and hot air pretreated samples were observed to be 62.63 % and 59.11% respectively on the wet basis. It was observed from the Fig. 3 that for the same roller speed, the average peeling efficiency was reported to be higher for hot air pretreated samples than the control ones.

The maximum peeling efficiency was observed to be 48.14% for hot air pretreated samples at 400 roller speed and minimum to be 33.89% at 300 roller speeds for control samples (Fig. 3). Similar results were reported by Manjunatha *et al.*, (2012) for the average peeling efficiencies at the corresponding moisture contents of 23.1, 27.7, 33.4 and 40.5%. The efficiencies reported were 79.71, 81.16, 78.27 and 68.73%.

The values of peeling efficiency increased with decrease in moisture content due to the loosening of garlic skin on tray drying. Moreover, loosening of skin reduced the damage and mashing of cloves. Statistically, it was found that pre-treatment was highly significant on the peeling efficiency.

Effect of rotational speed on peeling efficiency

Rotational speed of the roller has non significant effect on the peeling efficiency of garlic. It was observed from the Fig. 4 that the mean value of peeling efficiency increases with increase in rotational speed at constant batch load of ½ kg and constant peeling residence time of one minute. The minimum peeling efficiency was observed to be 33.89% at 300 rpm and maximum was 43.07% at 500 roller speed for control samples. For hot air pretreated samples, the minimum and maximum peeling efficiencies were 41.05% and 48.14% at 300 and 400 roller speeds respectively. Taking into account the combined factor, the combination of pretreatment and roller speed was significant.

Similar results were reported by Manjunatha *et al.*, (2012), that the peeling efficiency was higher at 36 rpm as compared to 42 and 29 rpm at 27.7% moisture content at all the three levels of cylinder concave clearance. It was due to the reason that at the lower rpms more damage occurs because of prolonged abrasion and impact of the roller. Moreover, higher rpm results in increase in efficiency but at the same time it causes physical rupture and mashing of cloves.

Effect of pretreatment on peeled clove recovery

Comparing the two samples- control and hot air, the peeled clove recovery for hot air pretreated samples was higher at one constant roller speed. Similar results were reported by Manjunatha *et al.*, (2012) that average peeled garlic cloves were found to be 78.49, 80.09, 76.89 and 65.76 % to the corresponding moisture contents of 23.1, 27.7, 33.4 and 40.5% respectively. Statistically, pre-treatment was found to be highly significant on the peeled clove recovery ($p < 0.05$) (Table 7). The peeling experiment was also run for

hot water blanched sample. It was found that the samples were in good condition but peeling in machine was not successful as the outer skin got adhered to the clove surface and abrasion principle did not work.

Effect of rotational speed on peeled clove recovery

The peeled clove recovery also exhibited the same trend as that of peeling efficiency. With an increase in the rotational speed of the roller, the peeled clove recovery also increased for control samples. For hot air pretreated samples, the trend observed was discontinuous. The effect of roller speed was found to be highly significant. With an increase from 300 rpm to 400 rpm in Fig. 4, the peeled clove recovery increased but with further increase from 400 to 500 rpm, the recovery decreased. It was due to the reason that increased rpm causes more abrasion and cloves get crushed as compared to at lower rpm's. The maximum peeled clove recovery calculated was 39.40% for hot air pretreated sample at 400 rpm and minimum of 27.50% at 300 rpm for control samples. The combination of pre-treatment and roller speed was also significant for the peeled clove recovery (Fig. 5 and 6).

Economic feasibility of developed garlic peeler

Economic analysis of garlic clove peeler was done to test the feasibility of machine taking into account the total cost which includes fixed cost and variable cost, returns, break-even point and payback period (Table 5).

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